



Fig. 4.

$C = -2$ , corresponding to  $K_0'' = -4.8 \times 10^{12}$  cm<sup>2</sup>/dyne. In spite of the impressive agreement, it should be mentioned that a phase transition at about 160 kb makes questionable any extrapolation from the low-pressure region into the high-pressure region.

The effect of varying  $m$  is shown in Figure 8 where we have plotted the calculated curves for aluminum oxide out to 5000 kb. Using values of  $m$  equal to 1, 2, and 3, equation 9 is plotted for  $C = -1$ . In addition, we have plotted the curves for  $m = 4.2, 5.2, 6.2$ , and  $C = +1.0$ . One can readily observe that the six curves are distinguishable only for extreme pressures. Also, as  $C \rightarrow 0$  for given  $K_0'$  and  $m$ , either  $a \rightarrow \infty$  or  $K_0' = m$ , and in both cases the limiting expression for  $K/K_0$  becomes independent of  $m$ . We may therefore conclude that the value of  $m$  does not appreciably affect the volume calculation when  $|C|$  is small.

As a final point of interest, Figure 9 compares typical results from equation 9 with re-

sults based on a quadratic approximation to the bulk modulus, given by

$$\frac{K}{K_0} = 1 + K_0'P + \frac{1}{2}CP^2$$

The extrapolation formula predicted by the quadratic approximation is obtained in a manner similar to that given in Appendix B for equation 7. That is

$$V = \exp \left[ - \int \frac{dP}{\frac{1}{2}CP^2 + K_0'P + 1} \right] \\ = \left\{ \frac{[CP + K_0' + (r)^{1/2}][K_0' - (r)^{1/2}]}{[CP + K_0' - (r)^{1/2}][K_0' + (r)^{1/2}]} \right\}^{1/(r^{1/2})} \quad (11)$$

where  $r = (K_0')^2 - 2C > 0$ . For  $r = 0$  and  $r < 0$  the volume equation becomes

$$V = \exp \left( \frac{2}{CP + K_0'} - \frac{2}{K_0'} \right) \quad (11a)$$

and

$$V = \exp \left\{ \right.$$

respectively. equations pr over a consi- tive values- flection poi- value of  $K$  at and at another

the bulk mod- addition, for 11a, and 11b

$$\left[ \frac{K_0'}{K_0'} - \right.$$

and